

GP-304338

OPTIMAL SELECTION OF INPUT TORQUE WITH STABILITY OF POWER FLOW FOR A HYBRID ELECTRIC VEHICLE

TECHNICAL FIELD

[0001] The present invention is related to control of a vehicular powertrain. More particularly, the invention is concerned with on-vehicle determinations of preferred operating points for the powertrain.

BACKGROUND OF THE INVENTION

[0002] Various hybrid powertrain architectures are known for managing the input and output torques of various prime-movers in hybrid vehicles, most commonly internal combustion engines and electric machines. Series hybrid architectures are generally characterized by an internal combustion engine driving an electric generator which in turn provides electrical power to an electric drivetrain and to a battery pack. The internal combustion engine in a series hybrid is not directly mechanically coupled to the drivetrain. The electric generator may also operate in a motoring mode to provide a starting function to the internal combustion engine, and the electric drivetrain may recapture vehicle braking energy by also operating in a generator mode to recharge the battery pack. Parallel hybrid architectures are generally characterized by an internal combustion engine and an electric motor which both have a direct mechanical coupling to the drivetrain. The drivetrain conventionally includes a shifting transmission to provide the necessary gear ratios for wide range operation.

[0003] Electrically variable transmissions (EVT) are known which provide for continuously variable speed ratios by combining features from both series and parallel hybrid powertrain architectures. EVTs are operable with a direct mechanical path between an internal combustion engine and a final drive unit thus enabling high transmission efficiency and application of lower cost and less massive motor hardware. EVTs are also operable with engine operation mechanically independent from the final drive or in various mechanical/electrical split contributions thereby enabling high-torque

continuously variable speed ratios, electrically dominated launches, regenerative braking, engine off idling, and multi-mode operation.

[0004] It is known to select engine power from the road-load power required plus an additional quantity of engine power based on the energy storage system's (e.g. battery's) state-of-charge. Following selection of engine power, the engine's optimal fuel economy or optimal emissions map or a combination thereof may be used to select the engine's torque/speed operating point. The battery power effected is that which is required, in combination with the engine power, to meet the road-load power requirements and to compensate for power losses within the system.

[0005] Known systems do not optimize the power flow of all the propulsion system components. Typically, only the engine operation is optimized. The prior art does not weigh additional factors such as other system mechanical and electrical losses and battery usage factors in selecting the overall system's preferred operating point.

[0006] A preferred method for determining input speed is disclosed in commonly assigned and co-pending United States patent application Serial Numbers 10/686,508 (Attorney Docket Number GP-304193) and 10/686,034 (Attorney Docket Number GP-304194). Therein, preferred operating points for a vehicle powertrain including an engine and a transmission are determined in accordance with a comprehensive operational mapping of input and output conditions and corresponding aggregate system losses corresponding to engine and transmission losses. In a hybrid transmission application, additional losses from motors and batteries are aggregated into the system losses and battery constraints are considered in determining preferred operating points. Preferred operating points are provided in one or more sets of minimized data for on-vehicle implementation. Desired input speed is provided by the system controller, for example in accordance with a desired operating point of the engine to meet various efficiency and emission objectives.

[0007] A preferred speed control for a hybrid transmission is described in detail in commonly assigned and co-pending United States patent application

Serial Number 10/686,511 (Attorney Docket Number GP-304140). Therein, a multi-mode hybrid transmission is described having speed control provided via an open loop model derived as a function of preselected transmission accelerations and controlled and uncontrolled transmission torques. Motor torques are selected as the controlled torques and other preselected transmission torques are selected as the uncontrolled torques. The control also employs a closed loop control effort responsive to at least one preselected transmission speed error.

SUMMARY OF THE INVENTION

[0008] The invention overcomes the deficiencies of the prior art by considering the system as a whole in determining operating conditions.

[0009] In accordance with one aspect of the present invention preferred operation of the system is achieved in accordance with considering the system as a whole in determining operating conditions.

[0010] In accordance with another aspect of the present invention optimum system operating points are determined through comprehensive consideration of engine, mechanical and electrical based contributory system losses.

[0011] In accordance with yet another aspect of the present invention optimum system operating points are determined with additional considerations of subjective factors related to battery usage.

[0012] A method for establishing a preferred operating point for a preselected powertrain operating parameter in a powertrain system includes determining a feasible operating space for the preselected powertrain operating parameter, searching the feasible operating space for a value corresponding to a minimum system power loss, and establishing the preferred operating point as the value corresponding to the minimum system power loss. Preferably, the preselected powertrain operating parameter is input torque. System power loss may include other factors not related to actual power loss but effective to bias the minimum power loss away from input torques that are less desirable because of other considerations such as battery use in a hybrid

powertrain. During quiescent powertrain operation, additional stability is achieved by requiring a predetermined level of power loss improvement from one preferred operating parameter determination to the next before any change in the preferred operating parameter is made. A preferred manner of searching the feasible operating space includes a section search performed in accordance with a golden section ratio.

BRIEF DESCRIPTION OF THE DRAWINGS

[0013] FIG. 1 is a mechanical hardware schematic representation of one preferred form of a two-mode, compound-split, electrically variable transmission particularly suited to the implementation of the present invention;

[0014] FIG. 2 is an electrical and mechanical schematic of a preferred system architecture for the hybrid powertrain disclosed herein;

[0015] FIG. 3 is a graphical representation of various regions of operation with respect to input and output speeds of the exemplary electrically variable transmission disclosed herein;

[0016] FIG. 4 is a torque space plot in motor torques (T_a and T_b) including exemplary lines of constant battery power (P_{batt}), exemplary lines of constant output torque (T_o) and exemplary lines of constant engine torque (i.e. input torque T_i);

[0017] FIG. 5 is a plot of exemplary individual sub-system costs and aggregate system costs correlated to power across an input torque range useful in determining an optimum input torque operating point at a set of current system speeds and accelerations;

[0018] FIG. 6 is a graphical representation of a preferred technique for converging on a minimum system cost operating point in input torque;

[0019] FIG. 7 is a graphical depiction of empirically determined motor torque vs. speed characteristic data utilized in the determination of feasible operating space in accordance with the present invention;

[0020] FIG. 8 is a graphical representation of battery power losses vs. battery power characteristic data utilized in the determination of battery power losses in accordance with the present invention;

[0021] FIG. 9 is a graphical representation of state of charge cost factors across the range of battery states of charge attributed to battery power flows and as utilized in the determination of battery utilization cost considered in the optimum input torque determination of the present invention;

[0022] FIG. 10 is a graphical representation of battery throughput cost factors across the range of battery throughput as utilized in the determination of battery utilization cost considered in the optimum input torque determination of the present invention; and,

[0023] FIG. 11 illustrates a flowchart of exemplary steps in a set of instructions executed by a computer based controller particularly related to determining an optimum powertrain operating parameter in accordance with the present invention;

[0024] FIG. 12 is a graphical depiction of empirically determined motor torque vs. speed characteristic data utilized in the determination of motor losses in accordance with the present invention; and,

[0025] FIGS. 13A and 13B illustrate a flowchart of exemplary steps in a set of instructions executed by a computer based controller particularly related to stability of power flow in accordance with the present invention.

DESCRIPTION OF THE PREFERRED EMBODIMENT

[0026] With reference first to FIGS. 1 and 2, a vehicular powertrain system is generally designated 11. Included in the powertrain 11 is one representative form of a multi-mode, compound-split, electrically variable transmission (EVT) particularly suited for implementing the controls of the present invention and designated generally by the numeral 10 in FIGS. 1 and 2. With particular reference, then, to those figures, the EVT 10 has an input member 12 that may be in the nature of a shaft which may be directly driven by an engine 14 or, as shown in FIG. 2, a transient torque damper 16 may be incorporated between the output member of the engine 14 and the input member of the EVT 10. The transient torque damper 16 may incorporate, or be employed in conjunction with, a torque transfer device (not shown) to permit selective engagement of the engine 14 with the EVT 10, but it must be

understood that such a torque transfer device is not utilized to change, or control, the mode in which the EVT 10 operates.

[0027] In the embodiment depicted the engine 14 may be a fossil fuel engine, such as a diesel engine which is readily adapted to provide its available power output delivered at a constant number of revolutions per minute (RPM). In the exemplary embodiment to which FIGS. 1 and 2 are directed, the engine 14 can - after start-up, and during the majority of its input - operate at a constant speed or at a variety of constant speeds in accordance with a desired operating point as may be determined from operator inputs and driving conditions.

[0028] The EVT 10 utilizes three planetary gear subsets 24, 26 and 28. The first planetary gear subset 24 has an outer gear member 30, that may generally be designated as the ring gear, which circumscribes an inner gear member 32, generally designated as the sun gear. A plurality of planet gear members 34 are rotatably mounted on a carrier 36 such that each planet gear member 34 meshingly engages both the outer gear member 30 and the inner gear member 32.

[0029] The second planetary gear subset 26 also has an outer gear member 38, generally designated as the ring gear, which circumscribes an inner gear member 40, generally designated as the sun gear. A plurality of planet gear members 42 are rotatably mounted on a carrier 44 such that each planet gear 42 meshingly engages both the outer gear member 38 and the inner gear member 40.

[0030] The third planetary gear subset 28 also has an outer gear member 46, generally designated as the ring gear, which circumscribes an inner gear member 48, generally designated as the sun gear. A plurality of planet gear members 50 are rotatably mounted on a carrier 52 such that each planet gear 50 meshingly engages both the outer gear member 46 and the inner gear member 48.

[0031] While all three planetary gear subsets 24, 26 and 28 are "simple" planetary gear subsets in their own right, the first and second planetary gear subsets 24 and 26 are compounded in that the inner gear member 32 of the

first planetary gear subset 24 is conjoined, as through a hub plate gear 54, to the outer gear member 38 of the second planetary gear subset 26. The conjoined inner gear member 32 of the first planetary gear subset 24 and the outer gear member 38 of the second planetary gear subset 26 are continuously connected to a first motor/generator 56, as by a sleeve shaft 58. First motor/generator 56 may also be referred to herein variously as motor A or MA.

[0032] The planetary gear subsets 24 and 26 are further compounded in that the carrier 36 of the first planetary gear subset 24 is conjoined, as through a shaft 60, to the carrier 44 of the second planetary gear subset 26. As such, carriers 36 and 44 of the first and second planetary gear subsets 24 and 26, respectively, are conjoined. The shaft 60 is also selectively connected to the carrier 52 of the third planetary gear subset 28, as through a torque transfer device 62 which, as will be hereinafter more fully explained, is employed to assist in the selection of the operational modes of the EVT 10. Torque transfer device 62 may also be referred to herein variously as second clutch, clutch two or C2.

[0033] The carrier 52 of the third planetary gear subset 28 is connected directly to the transmission output member 64. When the EVT 10 is used in a land vehicle, the output member 64 may be connected to the vehicular axles (not shown) that may, in turn, terminate in the drive members (also not shown). The drive members may be either front or rear wheels of the vehicle on which they are employed, or they may be the drive gear of a track vehicle.

[0034] The inner gear member 40 of the second planetary gear subset 26 is connected to the inner gear member 48 of the third planetary gear subset 28, as through a sleeve shaft 66 that circumscribes shaft 60. The outer gear member 46 of the third planetary gear subset 28 is selectively connected to ground, represented by the transmission housing 68, through a torque transfer device 70. Torque transfer device 70, as is also hereinafter explained, is also employed to assist in the selection of the operational modes of the EVT 10. Torque transfer device 70 may also be referred to herein variously as first clutch, clutch one or C1.

[0035] The sleeve shaft 66 is also continuously connected to a second motor/generator 72. Second motor/generator 72 may also be referred to herein variously as motor B or MB. All the planetary gear subsets 24, 26 and 28 as well as motor A and motor B (56, 72) are coaxially oriented, as about the axially disposed shaft 60. It should be noted that both motors A and B are of an annular configuration which permits them to circumscribe the three planetary gear subsets 24, 26 and 28 such that the planetary gear subsets 24, 26 and 28 are disposed radially inwardly of the motors A and B. This configuration assures that the overall envelope--i.e.: the circumferential dimension--of the EVT 10 is minimized.

[0036] A drive gear 80 may be presented from the input member 12. As depicted, the drive gear 80 fixedly connects the input member 12 to the outer gear member 30 of the first planetary gear subset 24, and the drive gear 80, therefore, receives power from the engine 14 and/or the motor/generators 56 and/or 72. The drive gear 80 meshingly engages an idler gear 82 which, in turn, meshingly engages a transfer gear 84 that is secured to one end of a shaft 86. The other end of the shaft 86 may be secured to a transmission fluid pump and 88 which is supplied transmission fluid from sump 37, delivering high pressure fluid to regulator 39 which returns a portion of the fluid to sump 37 and provides regulated line pressure in line 41.

[0037] In the described exemplary mechanical arrangement, the output member 64 receives power through two distinct gear trains within the EVT 10. A first mode, or gear train, is selected when the first clutch C1 is actuated in order to "ground" the outer gear member 46 of the third planetary gear subset 28. A second mode, or gear train, is selected when the first clutch C1 is released and the second clutch C2 is simultaneously actuated to connect the shaft 60 to the carrier 52 of the third planetary gear subset 28. As used herein, when a mode related to a gear train is referenced an upper case designation MODE 1 or MODE 2, or M1 or M2, will generally be used.

[0038] Those skilled in the art will appreciate that the EVT 10 is capable of providing a range of output speeds from relatively slow to relatively fast within each mode of operation. This combination of two modes with a slow to

fast output speed range in each mode allows the EVT 10 to propel a vehicle from a stationary condition to highway speeds. In addition, a fixed-ratio state wherein both clutches C1 and C2 are simultaneously applied is available for efficient mechanical coupling of the input member to the output member through a fixed gear ratio. Furthermore, a neutral state wherein both clutches C1 and C2 are simultaneously released is available for mechanically decoupling the output member from the transmission. Finally, the EVT 10 is capable to provide synchronized shifts between the modes wherein slip speed across both clutches C1 and C2 is substantially zero. Additional details regarding operation of the exemplary EVT can be found in commonly assigned United States Patent Number 5,931,757, the contents of which are incorporated herein by reference.

[0039] Engine 14 is preferably a diesel engine and electronically controlled by engine control module (ECM) 23 as illustrated in FIG. 2. ECM 23 is a conventional microprocessor based diesel engine controller comprising such common elements as microprocessor, read only memory ROM, random access memory RAM, electrically programmable read only memory EPROM, high speed clock, analog to digital (A/D) and digital to analog (D/A) circuitry, and input/output circuitry and devices (I/O) and appropriate signal conditioning and buffer circuitry. ECM 23 functions to acquire data from a variety of sensors and control a variety of actuators, respectively, of the engine 14 over a plurality of discrete lines. For simplicity, ECM 23 is shown generally in bi-directional interface with engine 14 via aggregate line 35. Among the various parameters that may be sensed by ECM 23 are oil sump and engine coolant temperatures, engine speed (N_e), turbo pressure, and ambient air temperature and pressure. Various actuators that may be controlled by the ECM 23 include fuel injectors, fan controllers, engine preheaters including glow plugs and grid-type intake air heaters. ECM preferably provides for well known torque based controls for engine 14 in response to a torque command T_{e_cmd} provided by the EVT control system. Such engine electronics, controls and quantities are generally well known to

those skilled in the art and further detailed exposition thereof is not required herein

[0040] As should be apparent from the foregoing description the EVT 10 selectively receives power from the engine 14. As will now be explained with continued reference to FIG. 2 the EVT also receives power from an electric storage device such as one or more batteries in battery pack module (BPM) 21. The powertrain system also includes such energy storage devices which are an integral part of the power flows thereof. Other electric storage devices that have the ability to store electric power and dispense electric power may be used in place of the batteries without altering the concepts of the present invention. The BPM 21 is high voltage DC coupled to dual power inverter module (DPIM) 19 via DC lines 27. Current is transferable to or from the BPM 21 in accordance with whether the BPM 21 is being charged or discharged. DPIM 19 includes a pair of power inverters and respective motor controllers configured to receive motor control commands and control inverter states therefrom for providing motor drive or regeneration functionality. Motor controllers are microprocessor based controllers comprising such common elements as microprocessor, read only memory ROM, random access memory RAM, electrically programmable read only memory EPROM, high speed clock, analog to digital (A/D) and digital to analog (D/A) circuitry, and input/output circuitry and devices (I/O) and appropriate signal conditioning and buffer circuitry. In motoring control, the respective inverter receives current from the DC lines and provides AC current to the respective motor over high voltage phase lines 29 and 31. In regeneration control, the respective inverter receives AC current from the motor over high voltage phase lines 29 and 31 and provides current to the DC lines 27. The net DC current provided to or from the inverters determines the charge or discharge operating mode of the BPM 21. Preferably, MA and MB are three-phase AC machines and the inverters comprise complementary three-phase power electronics. Individual motor speed signals Na and Nb for MA and MB, respectively, are also derived by the DPIM 19 from the motor phase information or conventional rotation sensors. Such motors, electronics,

controls and quantities are generally well known to those skilled in the art and further detailed exposition thereof is not required herein.

[0041] System controller 43 is a microprocessor based controller comprising such common elements as microprocessor, read only memory ROM, random access memory RAM, electrically programmable read only memory EPROM, high speed clock, analog to digital (A/D) and digital to analog (D/A) circuitry, digital signal processor (DSP), and input/output circuitry and devices (I/O) and appropriate signal conditioning and buffer circuitry. In the exemplary embodiment, system controller 43 comprises a pair of microprocessor based controllers designated as vehicle control module (VCM) 15 and transmission control module (TCM) 17. VCM and TCM may provide, for example, a variety of control and diagnostic functions related to EVT and vehicle chassis including, for example, engine torque commands, input speed control, and output torque control in coordination with regenerative braking, anti-lock braking and traction control. Particularly with respect to EVT functionality, system controller 43 functions to directly acquire data from a variety of sensors and directly control a variety of actuators, respectively, of the EVT over a plurality of discrete lines. For simplicity, System controller 43 is shown generally in bi-directional interface with EVT via aggregate line 33. Of particular note, system controller 43 receives frequency signals from rotation sensors for processing into input member 12 speed N_i and output member 64 speed N_o for use in the control of EVT 10. System controller 43 may also receive and process pressure signals from pressure switches (not separately illustrated) for monitoring clutch C1 and C2 application chamber pressures. Alternatively, pressure transducers for wide range pressure monitoring may be employed. PWM and/or binary control signals are provided by system controller to EVT 10 for controlling fill and drain of clutches C1 and C2 for application and release thereof. Additionally, system controller 43 may receive transmission fluid sump 37 temperature data, such as from conventional thermocouple input (not separately illustrated) to derive sump temperature T_s and provide a PWM signal which may be derived from input speed N_i and sump temperature T_s for control of line pressure via

regulator 39. Fill and drain of clutches C1 and C2 are effectuated by way of solenoid controlled spool valves responsive to PWM and binary control signals as alluded to above. Trim valves are preferably employed using variable bleed solenoids to provide precise placement of the spool within the valve body and correspondingly precise control of clutch pressure during apply. Similarly, line pressure regulator 39 may be of a solenoid controlled variety for establishing regulated line pressure in accordance with the described PWM signal. Such line pressure controls are generally well known to those skilled in the art. Clutch slip speeds across clutches C1 and C2 are derived from output speed N_o , MA speed N_a and MB speed N_b ; specifically, C1 slip is a function of N_o and N_b , whereas C2 slip is a function of N_o , N_a and N_b . Also illustrated is user interface (UI) block 13 which comprises such inputs to system controller 43 such as vehicle throttle position, push button shift selector (PBSS) for available drive range selection, brake effort and fast idle requests among others.

[0042] System controller 43 determines a torque command T_{e_cmd} and provides it to ECM 23. Torque command T_{e_cmd} is representative of the EVT torque contribution desired from the engine as determined by the system controller. System controller 43 also determines a speed command N_{e_des} representative of the EVT input speed desired, which in the direct coupled arrangement between the engine and the EVT is also the desired engine speed operating point. With the direct coupled arrangement exemplified herein, the engine torque and the EVT input torque, T_e and T_i respectively, are equivalent and may be referred to in the alternative herein. Similarly, the engine speed and the EVT input speed, N_e and N_i respectively, are equivalent and may be referred to in the alternative herein. Desired input speed operating points are preferably determined as disclosed in commonly assigned and co-pending United States patent application Serial Numbers 10/686,508 (Attorney Docket Number GP-304193) and 10/686,034 (Attorney Docket Number GP-304194) which are incorporated herein by reference. A preferred speed control for a hybrid transmission is described in detail in commonly assigned and co-

pending United States patent application Serial Number 10/686,511 (Attorney Docket Number GP-304140) which is incorporated herein by reference.

[0043] The various modules described (i.e. system controller 43, DPIM 19, BPM 21, ECM 23) communicate via controller area network (CAN) bus 25. The CAN bus 25 allows for communication of control parameters and commands between the various modules. The specific communication protocol utilized will be application specific. For example the preferred protocol for heavy duty applications is the Society of Automotive Engineers standard J1939. The CAN bus and appropriate protocols provide for robust messaging and multi-controller interfacing between the system controller, ECM, DPIM, BPIM and other controllers such as antilock brake and traction controllers.

[0044] With reference to FIG. 3, a plot of output speed N_o along the horizontal axis versus input speed N_i across the vertical axis for the EVT 10 is illustrated. Synchronous operation, that is the input speed and output speed relationships whereat both clutch C1 and C2 are operating simultaneously with substantially zero slip speed thereacross is represented by line 91. As such, it represents the input and output speed relationships substantially whereat synchronous shifting from between modes can occur or whereat direct mechanical coupling from input to output can be effected by simultaneous application of both clutches C1 and C2, also known as fixed-ratio. One particular gearset relationship capable of producing the synchronous operation depicted by line 91 in FIG. 3 is as follows: outer gear member 30 having 91 teeth, inner gear member 32 having 49 teeth, planet gear members 34 having 21 teeth; outer gear member 38 having 91 teeth, inner gear member 40 having 49 teeth, planet gear members 42 having 21 teeth; outer gear member 46 having 89 teeth, inner gear member 48 having 31 teeth, planet gear members 50 having 29 teeth. Line 91 may be variously referred to herein as synchronous line, shift ratio line or fixed-ratio line.

[0045] To the left of the shift ratio line 91 is a preferred region of operation 93 for the first mode wherein C1 is applied and C2 is released. To the right of the shift ratio line 91 is a preferred region of operation 95 for the

second mode wherein C1 is released and C2 is applied. When used herein with respect to clutches C1 and C2, the term applied indicates substantial torque transfer capacity across the respective clutch while the term released indicates insubstantial torque transfer capacity across the respective clutch. Since it is generally preferred to cause shifts from one mode to the other to occur synchronously, torque transfers from one mode into the other mode are caused to occur through a two clutch application fixed ratio wherein, for a finite period prior to the release of the presently applied clutch, the presently released clutch is applied. And, the mode change is completed when fixed-ratio is exited by the continued application of the clutch associated with the mode being entered and the release of the clutch associated with the mode being exited.

[0046] While region of operation 93 is generally preferred for the operation of the EVT in MODE 1, it is not meant to imply that MODE 2 operation of the EVT cannot or does not occur therein. Generally, however, it is preferred to operate in MODE 1 in region 93 because MODE 1 preferably employs gearsets and motor hardware particularly well suited in various aspects (e.g. mass, size, cost, inertial capabilities, etc.) to the high launch torques of region 93. Similarly, while region of operation 95 is generally preferred for the operation of the EVT in MODE 2, it is not meant to imply that MODE 1 operation of the EVT cannot or does not occur therein.

Generally, however, it is preferred to operate in MODE 2 in region 95 because MODE 2 preferably employs gearsets and motor hardware particularly well suited in various aspects (e.g. mass, size, cost, inertial capabilities, etc.) to the high speeds of region 93. Region 93, wherein MODE 1 operation is generally preferred, may be considered a low speed region whereas region 95, wherein MODE 2 operation is generally preferred, may be considered a high speed region. A shift into MODE 1 is considered a downshift and is associated with a higher gear ratio in accordance with the relationship of N_i/N_o . Likewise, a shift into MODE 2 is considered an upshift and is associated with a lower gear ratio in accordance with the relationship of N_i/N_o .

[0047] As a starting point for the present control, various powertrain parameters are measured or otherwise predetermined. Output speed, N_o , and input speed, N_i , are preferably derived from sensed and filtered signals. Motor speeds N_a and N_b are known through sensing, calculated with known coupling constraints of the EVT, or derived through the motor control phase information. Input acceleration, N_{i_dot} , is preferably a desired rate of change of transmission input speed determined as taught in commonly assigned and co-pending United States patent application Serial Number 10/686,511 (Attorney Docket Number GP-304140). Output speed acceleration, N_{o_dot} , is preferably determined in accordance with sensed and filtered output speed, N_o , also as disclosed in commonly assigned and co-pending United States patent application Serial Number 10/686,511 (Attorney Docket Number GP-304140).

[0048] Minimum and maximum motor torques (T_{a_min} , T_{a_max} , T_{b_min} and T_{b_max}) within the present condition capabilities of the motors are preferably obtained from data sets stored in table form within data structures in system controller 43. Such data sets are provided for reference by the routine in pre-stored table format having been empirically derived from conventional dynamometer testing of the combined motor and power electronics (e.g. power inverter) at various temperature and voltage conditions. An exemplary representation of such characteristic motor torque vs. speed data is illustrated in FIG. 7 wherein minimum and maximum data for a given speed are represented by the line of constant speed 112 intersecting exemplary lines of constant temperature/voltage 111, 113. The tabulated data is referenced by the motor speed (N_a , N_b), voltage and temperature. Motor speeds can be derived from the input speed N_i and output speed N_o in accordance with the following known coupling constraint equation:

$$\begin{bmatrix} N_a \\ N_b \end{bmatrix} = \begin{bmatrix} K_{11} & K_{12} \\ K_{21} & K_{22} \end{bmatrix} \begin{bmatrix} N_i \\ N_o \end{bmatrix}$$

where N_a is motor A speed,

N_b is motor B speed,

N_i is EVT input speed,

N_o is EVT output speed, and

K_n is a 2x2 matrix of parametric values determined by the hardware gear and shaft interconnections.

[0049] While the motors are used in both motoring and generating modes - suggesting four-quadrants (I, II, III, IV) of torque/speed data - two quadrant data collection is generally sufficient wherein the data collected in adjacent quadrants is merely reflected in the other quadrants not directly measured. In the present example, quadrants I and II are shown with determined data 111 whereas quadrants III and IV are shown populated with reflected data 113 therefrom.

[0050] Minimum and maximum battery power, P_{batt_min} and P_{batt_max} , within the present condition capabilities of the batteries are preferably obtained from data sets stored in table form within data structures in system controller 43. Such data sets are provided for reference by the routine in pre-stored table format having been correlated to various conditions, e.g. state of charge, temperature, voltage and usage (amp-hour/hour). A preferred method of determining minimum and maximum battery power is disclosed in commonly assigned and co-pending United States patent application Serial Number 10/686,180 (Attorney Docket Number GP-304119) which is incorporated herein by reference.

[0051] With reference now to FIG. 4, motor a (M_A) torque is plotted across the horizontal axis and motor b (M_B) torque is plotted across the vertical axis. Boundaries are drawn as dotted lines corresponding to minimum and maximum motor A torques (T_{a_min} and T_{a_max}), the minimum and maximum being with respect to motor capabilities at certain exemplary present operating conditions in N_i , N_o , N_{i_dot} and N_{o_dot} , the precise values of which are not required for the present exposition of the teachings to be gained from FIG. 4 and the present discussion. Similar boundaries are drawn as dotted lines corresponding to such minimum and maximum motor B

torques (T_{b_min} and T_{b_max}). The enclosed space represents a feasible solution space at present conditions for the motor units MA and MB. Once again, the precise values used herein are not critical to the understanding to be gained from the present description and figure, but are provided for appropriate context and to reduce the teaching's abstraction.

[0052] Within this motor torque solution space are plotted several other parameter lines of constant values which similarly are provided with exemplary values which are not critical to the understanding to be gained from the present description and figure but which are provided for appropriate context and reduction in abstraction of the present teaching. A plurality of lines of constant battery power, P_{batt} , are plotted which represent constant battery power solutions within the feasible solution space in T_a and T_b . Also plotted within this motor torque solution space are lines of constant output torque, T_o , which represent constant output torque solutions within the feasible solution space in T_a and T_b . Finally, lines of constant input torque are plotted within the same feasible solution space in T_a and T_b and represent constant input torque solutions therein. In the graphic representation of FIG. 4, while the space with respect to T_a and T_b is feasible in accordance with the capabilities of the respective motor units, the lines of constant battery power (P_{batt}), lines of constant output torque (T_o) and lines of constant input torque (T_i) are not necessarily representative of feasible solutions with respect to their respective subsystem capabilities at present conditions. But for the sake of clarity in FIG. 4, the lines of constant input torque, T_i , are limited to feasible solutions of input torques, e.g. -400 Nm to 1000 Nm in the present example.

[0053] With continued reference to FIG. 4, a desired output torque, T_{o_des} , is plotted and represented in the figure as a thick solid line. T_{o_des} represents the system constrained output torque target for the control. It may correspond to the torque requested by the vehicle operator in the event that the request is within the system's capabilities. But it may correspond to a constrained output torque in accordance with system limits. T_{o_des} may also be constrained in accordance with other factors apart from system capabilities

such as vehicle driveability and stability considerations. Constrained output torques may be determined in accordance with minimum and maximum input torque capabilities at present operating conditions (T_{i_min} , T_{i_max}), minimum and maximum motor torques at present operating conditions (T_{a_min} , T_{a_max} , T_{b_min} , T_{b_max}) and minimum and maximum battery power capabilities at present operating conditions (P_{batt_min} , P_{batt_max}).

[0054] It is along this T_{o_des} line that the feasible solution space within T_a and T_b is presently relevant. Similarly, it is along this T_{o_des} line that the feasible input torques, $-400 \text{ Nm} > T_i > 1000 \text{ Nm}$ are presently relevant. It is also along this T_{o_des} line that the feasible battery powers, $P_{batt_min} > P_{batt} > P_{batt_max}$ are presently relevant. The overall feasible solution space for T_{o_des} , therefore, is variously bounded by present capabilities as presented as minimum and maximum motor unit torques, input torques, and battery powers.

[0055] Within this feasible solution space it is desirable to determine an optimum operating point for input torque. A preferred method for determining input torque within a feasible solution space as described is set forth below in reference to the flow chart of FIG. 11. The flow chart illustrates representative steps for carrying out the method of the present invention comprising instructions implemented as part of the executable computer code and data structures of system controller 43. The instructions represented thereby are, of course, executed as a part of a much larger group of instruction sets and routines carrying out the various control and diagnostic function of the powertrain previously described.

[0056] Beginning with step 131 the operator request for output torque is determined. Preferably, a torque request is resolved from a plurality of operator inputs including: accelerator pedal position, brake pedal position and shift selector position; vehicle dynamic conditions such as acceleration rate or deceleration rate; and, EVT operational conditions such as temperatures, voltages, currents and speeds.

[0057] At step 132 the desired output torque (T_{o_des}) is determined. The requested torque from step 131 is evaluated and subjected to a variety of limit

tests to ensure that the resultant desired output torque is within various system constraints. The constraints include input torque maximums and minimums as determined in accordance with present operating conditions for the engine including predominantly actual engine speed N_e (input speed N_i). The constraints further include motor minimum and maximum torques and minimum and maximum battery powers.

[0058] A section search is preferably performed with the objective of quickly converging upon a preferred input torque operating point as described below. Within the maximum and minimum input torque limits, T_{i_min} and T_{i_max} , already established, an evaluation input torque, T_{i_n} , is selected at step 133. Evaluation input torque are preferably established in accordance with the well known golden section ratio wherein the entire range of remaining feasible input torques, (T_{i_min} to T_{i_max} in the initial iteration) is effectively divided into two regions having the ratios Φ and $1 - \Phi$ with respect to the whole region wherein

$$\Phi = (\sqrt{5} - 1) / 2 \text{ which is approximately equal to } 0.61803\dots$$

In subsequent iterations, the Φ ratio section is measured off with respect to a newly established boundary of the region to be evaluated as explained at a later point more fully in conjunction with the illustration of FIG. 6.

[0059] At step 134, battery power P_{batt} is next determined at the selected evaluation input torque, T_{i_n} . The following coupling constraint equation is known for the EVT for calculating the motor A and motor B torques:

$$\begin{bmatrix} T_a \\ T_b \end{bmatrix} = \begin{bmatrix} K_{11} & K_{12} & K_{13} & K_{14} \\ K_{21} & K_{22} & K_{23} & K_{24} \end{bmatrix} \begin{bmatrix} T_i \\ T_o \\ N_{i_dot} \\ N_{o_dot} \end{bmatrix}$$

where T_a is motor A speed;

Tb is motor B speed;

Ti is EVT input speed;

To is EVT output speed;

Ni_dot is EVT input acceleration;

No_dot is EVT output acceleration; and

Kn is a 2x4 matrix of parametric values determined by the hardware gear and shaft interconnections and estimated hardware inertias applicable to the current drive range and represents what is commonly referred to as the plant model.

Additionally, motor speeds are derived from the following known coupling constraint equation:

$$\begin{bmatrix} Na \\ Nb \end{bmatrix} = \begin{bmatrix} K_{11} & K_{12} \\ K_{21} & K_{22} \end{bmatrix} \begin{bmatrix} Ni \\ No \end{bmatrix}$$

where Na is motor A speed;

Nb is motor B speed;

Ni is EVT input speed;

No is EVT output speed; and

Kn is a 2x2 matrix of parametric values determined by the hardware gear and shaft interconnections.

Battery power at the evaluation input torque is determined in accordance with the following relationship:

$$P_{batt} = P_{motor_A} + P_{loss_A} + P_{motor_B} + P_{loss_B} + P_{loss_acc}$$

where P_{motor_A} and P_{motor_B} are unit A and unit B motor power, respectively;

P_{loss_A} and P_{loss_B} are unit A and unit B aggregate motor and power electronics losses (motor losses), respectively; and

Ploss_acc is modeled as a DC load, e.g $V \cdot I$, representing battery draw to power accessories or any other load upon the batteries not directly related to the motor units A and B.

Motor powers are determined in accordance with the following relationships:

$$P_{\text{motor_A}} = T_a \cdot N_a, \text{ and}$$

$$P_{\text{motor_B}} = T_b \cdot N_b$$

where motor speeds, N_a and N_b , and motor torques, T_a and T_b , are derived from the two coupling constraint equations shown above.

[0060] Motor losses are provided for reference by the routine in pre-stored table format indexed by the motor torque and motor speed, having been empirically derived from conventional dynamometer testing of the combined motor and power electronics (e.g. power inverter). An exemplary representation of such characteristic motor torque vs. speed data is illustrated in FIG. 12. The tabulated data is referenced by the motor torque (T_a , T_b) and motor speed (N_a , N_b). The difference between the electrical power input ($I_a \cdot V$ and $I_b \cdot V$) and the motor shaft mechanical power output ($T_a \cdot N_a$ and $T_b \cdot N_b$) equates to the motor power loss ($P_{\text{loss_A}}$, $P_{\text{loss_B}}$) as follows:

$$P_{\text{loss_A}} = I_a \cdot V - P_{\text{motor_A}}; \text{ and}$$

$$P_{\text{loss_B}} = I_b \cdot V - P_{\text{motor_B}}$$

where I_a and I_b are the currents delivered to motor A and motor B power inverters, respectively; and

V is the voltage at which the currents are provided.

[0061] While the motors are used in both motoring and generating modes - suggesting four-quadrants (I, II, III, IV) of torque/speed data - two quadrant data collection is generally sufficient wherein the data collected in adjacent quadrants is merely reflected in the other quadrants not directly measured. In the present example, quadrants I and II are shown with determined data 151

whereas quadrants III and IV are shown populated with reflected data 153 therefrom.

[0062] At this point at step 135 performs an evaluation of the battery power P_{batt} just determined by comparing the battery power to the battery power constraints or limits, P_{batt_min} and P_{batt_max} , at the present conditions. If battery power for the evaluated input torque is not within the limits, then the routine skips to step 138 whereat the present evaluation input torque Ti_n establishes a new input torque boundary for the range of remaining feasible input torques to be evaluated. An acceptable battery power otherwise results in control passing to cost estimation step 136 whereat various subsystem power losses and other subjective costs are determined for the evaluation input torque.

[0063] One objective of the present step 136 is to determine an overall system power loss comprising a summation of individual subsystem power losses as follows:

$$P_{loss_total} = P_{loss_evt} + P_{loss_eng} + P_{loss_A} + P_{loss_B} + P_{loss_batt}$$

where P_{loss_evt} represents EVT losses such as hydraulic pumping loss, spin loss, clutch drag, etc.;

P_{loss_eng} represents engine losses associated with operating away from the most efficient Brake Specific Fuel Consumption (BSFC) point;

P_{loss_A} represents motor A losses;

P_{loss_B} represents motor B losses; and,

P_{loss_batt} represents internal power losses for the batteries.

[0064] The EVT losses (P_{loss_evt}) are provided for reference by the routine in pre-stored table format indexed by Ni and No , having been empirically derived from conventional dynamometer testing of the EVT unit throughout its various modes of operation and within the effective gear ratio ranges associated therewith.

[0065] The engine power losses (Ploss_eng) also are determined in accordance with pre-stored tabulated data. The engine power losses are provided for reference by the routine in pre-stored table format indexed by Ti and Ni. The preferred manner of generating such tables is through application of a loss equation as follows for calculation of engine power loss:

$$P_{loss_eng} = \eta_{MAX} LHV (kJ/g) Q_{FUEL} (g/s) - P_{OUT}$$

where η_{MAX} is the engine's maximum efficiency,
 $LHV (kJ/g)$ is the fuel's lower heating value,
 $Q_{FUEL} (g/s)$ is the fuel flow rate at operational conditions, and
 P_{OUT} is the engine mechanical shaft output power at operational conditions.

Conventional dynamometer testing is employed to establish the baseline η_{MAX} and in the gathering and tabulation of the relative engine losses. Ploss_evt and Ploss_eng may also be combined into a single mechanical loss term or grouped together and referred to as Ploss_eng.

[0066] The motor losses are determined, stored and referenced as previously described.

[0067] The internal power loss for batteries, Ploss_batt, are commonly referred to as I^2R losses. Ploss_batt data are provided for reference by the routine in pre-stored table format generated from battery equivalence models and indexed by battery power, Pbatt. An exemplary representation of such characteristic battery power vs. loss data 115 is illustrated in FIG. 8.

[0068] Exemplary subsystem power losses are illustrated across an exemplary input torque region in FIG. 5.

[0069] Continuing at step 136 and with further reference to FIGS. 9 and 10, additional subjective costs are preferably calculated to be factored into the selection of an optimum input torque operating point in accordance with the present invention. Subjective costs are penalties, unlike the subsystem power

losses described up to this point, cannot be derived from physical loss models, but rather represent another form of penalty against operating the system at particular points. But these penalties are subjectively scaled with units of power loss so they can be factored with the subsystem losses described above. A first battery cost factor term, SOC_cost_Factor, penalizes charging at high states of charge (solid line 123 in FIG. 9) and penalizes discharging at low states of charge (broken line 121 in FIG. 9). A second battery cost factor term, Throughput_Cost_Factor, captures the effect of battery age and assigns appropriate penalties thereto (line 125 in FIG. 10). Battery age is preferably measured in terms of average battery current (Amp-hr/hr), and a penalty placed on average battery current operating points that increases with higher battery current. Such cost factors are preferably obtained from data sets stored in table form within data structures in system controller 43. Such data sets are provided for reference by the routine in pre-stored table format. The product of the respective cost factors and battery power yields the cost function terms, Pcost_SOC and Pcost_throughput. Additional details surrounding subjective cost factors are disclosed in commonly assigned and co-pending United States provisional patent application Serial Number 60/511,456 (Attorney Docket Number GP-304118) which is incorporated herein by reference.

[0070] The total subjective cost is determined in accordance with the summation of the individual subjective costs in the following example of SOC and throughput penalties:

$$Pcost_sub = Pcost_SOC + Pcost_throughput$$

where $Pcost_SOC = Pbatt * SOC_Cost_Factor$; and

$$Pcost_throughput = Pbatt * Throughput_Cost_Factor$$

Of course, Pcost_sub is scaled into the same units as the subsystem power losses described above. Pcost_sub is therefore similarly seen plotted in FIG. 5 across the exemplary input torque region.

[0071] The total loss, $Total_loss$, is then determined as the summation of the subsystem power losses of $Ploss_total$ and the scaled subjective cost penalties of $Pcost_sub$ as follows:

$$Total_loss = Ploss_total + Pcost_sub$$

$Total_loss$ is therefore similarly seen plotted in FIG. 5 across the exemplary input torque region.

[0072] Step 137 is next encountered whereat a comparison of the $Total_loss$ determined at the evaluation input torque, Ti_n , is compared with the $Total_loss$ determined at the previous evaluation torque, Ti_n-1 . A first instance through the routine which would have no such prior $Total_loss$ determination would simply result in the return of the routine to step 133 whereat a second evaluation input torque would be determined in accordance with the golden section ratio considerations.

[0073] Step 138 eliminates solution space in input torque to the outside of the one of the evaluation input torques, Ti_n and Ti_n-1 , associated with the larger of the respective $Total_loss$ values corresponding thereto. The evaluation input torque, Ti_n or Ti_n-1 , associated with the larger of the respective $Total_loss$ values is then established as a new input torque boundary for the range of remaining feasible input torques to be evaluated.

[0074] Step 139 next determines if a predetermined number of iterations through the section search has been performed. If not, then the routine returns to step 133 to select another evaluation torque and loop through the routine steps 133-139. When the predetermined number of iterations has been accomplished, then step 140 is encountered whereat the optimum input torque, Ti_opt , is set the one of the current and immediate past evaluation input torques, Ti_n or Ti_n-1 , having the corresponding smallest $Total_loss$ associated therewith. The selected value for input torque is now available for use in setting the engine torque. But additional routines related to stability considerations at quiescent conditions are represented at step 141 which reduce the occurrence of frequent torque split changes which may be

objectionable. An exemplary quiescent stability routine is explained below in reference to FIGS 13A and 13B.

[0075] A section search performed in accordance with the described golden section ratio reduces the range of feasible input torques upon each subsequent evaluation by a factor of $1-\Phi$, or approximately 0.38197. Accuracy to within less than 1.0% can be established with eleven such evaluations. Modern engine controls are typically limited to control accuracy of substantially 1.0%. Evaluations beyond eleven are not presently believed to be of significant benefit. Hence, eleven such evaluations with the preferred golden section ratio search is the preferred number of evaluations performed.

[0076] Turning now to FIG. 6, an exemplary continuum of a range of input torques scaled between 0 and 1 appears across the horizontal axis. The initial range of the solution space in T_i corresponds to the T_{i_min} value (scaled to 0) and the T_{i_max} value (scaled to 1). Corresponding scaled and shifted Total_loss data are plotted against the vertical axis. A first comparison in accordance with the golden section ratio search would correspond to the pair of evaluation input torques associated with lines T_{i_1} and T_{i_2} . Visual inspection confirms that Total_loss at T_{i_2} is greater than Total_loss at T_{i_1} . Hence, the solution space to the outside of T_{i_2} is eliminated from further consideration (elimination A) and the new solution space corresponds to the limits of T_{i_min} and T_{i_2} (i.e. T_{i_2} is the new T_{i_max}). In accordance with the golden section ratio criteria, another evaluation input torque is established at T_{i_3} relative to the newest limit T_{i_2} . The lowest Total_loss from the previous iteration corresponding to T_{i_1} is compared to the Total_loss from the current iteration corresponding to the newest evaluation input torque, T_{i_3} . Again from visual inspection it can be appreciated that Total_loss at T_{i_3} is greater than Total_loss at T_{i_2} . Hence, the solution space to the outside of T_{i_3} is eliminated from further consideration (elimination B) and the new solution space corresponds to the limits of T_{i_3} and T_{i_2} (i.e. T_{i_3} is the new T_{i_min}). Once again, in accordance with the golden section ratio criteria, another evaluation input torque is established at T_{i_4} relative to the newest limit T_{i_3} . The lowest Total_loss from the previous iteration corresponding to

Ti_1 is compared to the Total_loss from the current iteration corresponding to the newest evaluation input torque, Ti_4. Again from visual inspection it can be appreciated that Total_loss at Ti_2 is greater than Total_loss at Ti_4. Hence, the solution space to the outside of Ti_2 is eliminated from further consideration (elimination C) and the new solution space corresponds to the limits of Ti_1 and Ti_2 (i.e. Ti_1 is the new Ti_min). This process is repeated consistently as described for a predefined number of iterations or comparisons at which point the optimum input torque is established as the one of the last two evaluation input torques corresponding to the smallest of the respective Total_loss values.

[0077] Alternative section searches can be employed in similar fashion to converge to an optimum input torque however with lesser efficiencies and uncertainties of reaching particular target accuracies within a known number of iterations or comparisons. Various other methods of solution convergence are also well known and applicable for implementation with the present invention including non-limiting examples of quadratic and other higher-order polynomial estimations and iterative derivative convergence techniques.

[0078] The quiescent stability routine begins in FIG. 13A by checking the state of a quiescent condition flag. A true flag state is indicative of a prior loop quiescent condition while a false state indicates no prior loop quiescent condition. Quiescent condition as used herein is determined by relatively low throttle pedal positions and relatively low vehicle speeds, both of which are preferably determined in accordance with calibratable thresholds. A true flag will pass to step 144 whereat a quiescent timer will be decremented. If the quiescent timer is expired then step 146 will pass control to step 149 whereat the quiescent flag is set to false thus indicating an end of quiescent condition management at this loop. Thereafter, Total_loss for the current loop is set exactly as determined back at the routine of FIG. 11 without any penalty or offset. If the quiescent timer has not expired as determined at step 146, then a check at step 148 is performed on the conditions defining a quiescent state. If quiescent conditions are not present then control similarly passes to step 149 whereat the quiescent flag is set to false thus indicating an end of quiescent

condition management at this loop. Thereafter, Total_loss for the current loop is set exactly as determined back at the routine of FIG. 11 without any penalty or offset. Steps 146 and 148 effectively terminate the quiescent management at the present loop if either the quiescent timer expires or the quiescent conditions are no longer present. If neither of those exit conditions is met, then step 151 is executed to assign a penalty or offset, K, to Total_loss determined back at the routine of FIG. 11.

[0079] Returning to step 142, a false flag passes control to step 143 whereat a check is performed on the conditions defining quiescent state. If quiescent conditions are not current then control passes to block 149 whereat the quiescent flag is set to false. Thereafter, Total_loss for the current loop is set exactly as determined back at the routine of FIG. 11 without any penalty or offset. If, however, the quiescent conditions are present, then steps 145 and 147 initialize the quiescent timer and set the quiescent flag to true, respectively. Thereafter, control passes to step 151 whereat a penalty or offset, K, is applied to Total_loss determined back at the routine of FIG. 11.

[0080] Therefore, quiescent conditions will for at least a predetermined duration result in a penalty or offset being applied to the current loop Total_loss whereas no current quiescent conditions or expiration of the predetermined duration will result in no such penalty or offset being applied. Furthermore as can be seen from FIG. 13A, subsequent to block 150, i.e. expired quiescent timer or no current quiescent conditions, the routine returns and no quiescent condition management steps are taken. But if the quiescent timer has not expired, quiescent conditions are still current and a penalty or offset to Total_loss is applied, then quiescent condition management steps are taken as set out in FIG. 13B.

[0081] With respect to the penalty or offset, K, a constant value may be selected for application for Total_loss values of multiple loops executed during the quiescent conditions duration or quiescent timer duration. However, it is also envisioned that the penalty or offset applied may decay for each of subsequent loops during the quiescent conditions duration or quiescent timer duration.

[0082] In FIG. 13B, the optimum input torque for the immediately preceding loop, Ti_opt_prior , is retrieved from memory at step 152. Thereafter, step 153 determines the battery power for current conditions at an input torque corresponding to the optimum input torque for the immediately preceding loop, $Pbatt@Ti_opt_prior$. The methodology for calculating battery power in the present routine is identical to that described with respect to the routine of FIG. 11, more particularly with respect to the description provided for step 134 thereof. Next, $Pbatt@Ti_opt_prior$ is compared to the minimum and maximum battery power limits at current conditions. This step, too, is accomplished with the same methodology as that described with respect to the routine of FIG. 11, more particularly with respect to the description provided for step 135 thereof. Where $Pbatt@Ti_opt_prior$ is outside of the limits thus indicating an infeasible battery power condition if Ti_opt_prior were utilized in the control of the EVT, control passes to step 157 whereat the input torque selected for control of the EVT is the optimum input torque corresponding to the present loop, Ti_opt . But where $Pbatt@Ti_opt_prior$ is feasible, step 155 is encountered and the various subsystem power losses and subjective costs are determined for current conditions at an input torque corresponding to the optimum input torque for the immediately preceding loop, $Total_loss@Ti_opt_prior$. Next at step 156 $Total_loss$ for the present loop, which in the case of the quiescent condition management steps of the present routine includes the penalty or offset, is compared to $Total_loss@Ti_opt_prior$. Then at step 157 the one of the optimum input torques, Ti_opt or Ti_opt_prior , corresponding to the smaller of the total losses, $Total_loss$ or $Total_loss@Ti_opt_prior$, is then selected as the optimum input torque to be returned for use in the control of the EVT. Therefore, as can be appreciated, the penalty or offset added to the present loop total loss will bias the system away from changing the input torque to a new setpoint during quiescent conditions unless there is a significant enough improvement in $Total_loss$ to be gained thereby or enough time has passed since the last input torque change that the frequency of input torque change is not objectionable.

[0083] The present invention has been described with respect to a particular exemplary hybrid powertrain arrangement. Those skilled in the art will recognize that other hybrid and conventional powertrain arrangements can be used in conjunction with the present invention. For example, conventional electro-hydraulically controlled, multi-speed transmissions can be used in conjunction with the present invention.

[0084] While the invention has been described by reference to certain preferred embodiments and implementations, it should be understood that numerous changes could be made within the spirit and scope of the inventive concepts described. Accordingly, it is intended that the invention not be limited to the disclosed embodiments, but that it have the full scope permitted by the language of the following claims.